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# Hydrogenation of $NO_x$ into ammonia under ambient conditions: From mechanistic investigation to multiphase catalysis

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#### ABSTRACT

This work proposes a NOx recycling approach through nitrite hydrogenation into ammonia (NH $_3$ /NH $_4$ OH), and the screened out Pd $^0$ /Pd $^2$ +-loaded heterogeneous catalyst achieves excellent ammonia yield. Initially, the DFT calculation of nitrite hydrogenation was conducted to study the determining step for N $_2$ /ammonia generation and guide the catalyst design. Consequently, the designed Pd $^2$ +-/ $^0$ /Covalent Triazine Framework (CTF) presented 100% nitrite conversion with 100% ammonia selectivity. The XPS and H $_2$ -TPR results demonstrated the Pd $^2$ +/Pd $^0$  ratios and Pd $^2$ + reducibility greatly affected the nitrite conversion and ammonia selectivity. DRIFTs examined the reaction intermediates and the impact of Pd distribution behind ammonia generation. Under ambient conditions, a model test from NOx adsorption to ammonia release has been completed, and it exhibited an overall conversion of 70% NOx into ammonia in a single cycle with TOF of 3.9 h $^{-1}$ , which proposes a direction of NOx recycling and utilization with less energy consumption and free of CO $_2$  emissions.

#### 1. Introduction

Nowadays, recycling exhaust gases (CO2, CHx, NOx and et al.) as resources to synthesize valuable chemicals could reduce the direct air pollution from exhaust gases emission and relieve supplying pressure for specific chemicals. NOx pollutants in the atmosphere mainly come from stable source (power plant and et al.) and mobile source (vehicles and et al.), and their annual emissions are above 10 million tons worldwide, which causes acid mist, acid rain, and ozone destruction and harms the human respiration system [1-3]. There have been many NOx elimination technologies according to NOx emission source, such as selective catalytic reduction by ammonia (NH3-SCR) or NOx storage and reduction (NSR), which convert NOx into N2 and release directly [4,5]. Considering the nitrogen cycle in an ecosystem (Schematic 1a), directly turning NOx into nitrates, nitrites, ammonium ion or other nitrogenous products as resources greatly save energy consumption for nitrogen fixation and across N<sub>2</sub> (N≡N bond energy: 941 kJ/mol) hydrogenation into ammonia [6]. For instance, if NOx from stable sources such as power stations could be utilized as the nitrogen source and transformed into ammonia through electro-catalysis method for fertilizer production, this will distinctly restrains NOx emissions and provide alternative approach for ammonia production simultaneously.

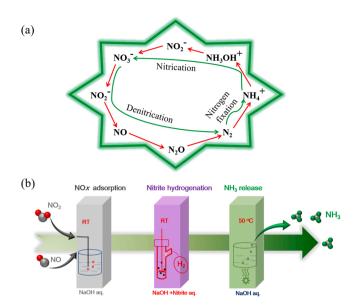
Long and et al. proposed NO reduction route into ammonia through electro-catalysis method, which was more active than N2 reduction route. Cu foam electrode was screened out to be the optimal active catalyst for NO reduction, and the ammonia generation rate achieved a state-of-the-art 517.1 μmol·cm<sup>-1</sup>·h<sup>-1</sup>. The highest Faradaic efficiency was 93.5% at -0.9 V potential, while the  $N_2$  and  $N_2O$  started to appear with time on stream. The calculation results demonstrated the superior ammonia selectivity was induced by favorable potentials for ammonia generation over copper electrode [7]. Besides, other experimental or theoretical calculation literatures also dedicated to explore stable catalysts and enhance catalytic performance and ammonia yield through reaction conditions optimization [8–10]. Nevertheless, the inferior NOxsolubility in aqueous system limits the ammonia total yield and the pH value of solution normally affects the reduction products distribution and reaction equilibrium. It is well known that NOx adsorption in basic solution could turn into nitrites according to Eq. (1), which presents excellent solubility and gives a good indication to boost ammonia total

$$NO_2 + NO + 2 NaOH = 2 NaNO_2 + H_2O$$
 (1)

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**Schematic 1.** (a) Simplified scheme of the "classical" nitrogen cycle. (b)  $NO_x$  recycling as resource through selective hydrogenation of nitrite into ammonia under ambient conditions.

$$NaNO_2 + 3 H_2 = NH_3 \cdot H_2O + NaOH$$
 (2)

$$2 \text{ NaNO}_2 + 3 \text{ H}_2 = \text{N}_2 + 2 \text{ NaOH} + 2 \text{ H}_2\text{O}$$
 (3)

$$2 \text{ NaNO}_2 + 5 \text{ H}_2 = \text{N}_2 \text{H}_4 + 2 \text{ NaOH} + 2 \text{ H}_2 \text{O}$$
 (4)

The nitrites/nitrates hydrogenation has been widely studied through thermo-catalysis, electro-catalysis and photo-catalysis methods so far [11,12]. In the beginning, nitrates hydrogenation is applied to eliminate the nitrogenous pollutants in the sewage treatment, and the N2 is the desired products for its nontoxicity and ammonia is considered as undesired by-product. Pintar and et al. used Pd/Cu bimetallic catalyst to eliminate nitrates from water, and it was documented the nitrites was the intermediates for nitrates hydrogenation. The presence of nitrites would not affect the N2 selectivity, while the increment of pH value could inhibit nitrates reaction rates [13,14]. Subsequently, nitrites/nitrates hydrogenation is utilized to synthesize ammonia, especially by electro-catalysis method. Ren and et al. prepared Cu@Cu2+1O nanowires and used it for electroreduction of nitrates to ammonia, and the ammonia yield rate achieved 576.53 µg⋅h<sup>-1</sup>⋅mg<sub>cat</sub><sup>-1</sup> and ammonia Faradaic efficiency was 87.07% at potential  $-1.2\,V$  vs. saturated calomel electrode [15]. Besides, Wei et al. report that both nitrate and nitrite can be hydrogenated to ammonia by dinickel phosphide with up to 96% selectivity [16]. The related studies about nitrates/nitrites reduction to ammonia mainly focus on efficient catalysts exploration through screening the active metals and supports, controlling the metal distribution and so on, while the nitrates/nitrites conversion and ammonia selectivity still needed to be further improved [17-20].

Combining the above nitrites/nitrates literatures progress, it is seen that the reactants concentrations are low and the solution pH value affects the  $N_2$  or ammonia selectivity. In order to improve the potential for ammonia production in aqueous system, we design an alternative approach in Schematic 1b to achieve a record ammonia yield through nitrite hydrogenation utilizing NOx as resources. Primarily, transform gaseous NOx is transformed into nitrite through NOx adsorption in alkaline solution, and then the nitrite in absorbent solution is hydrogenated to ammonia directly over a heterogeneous catalyst under ambient conditions. The advantages for this approach are no pollutants emission directly since the alkaline solution could be cycled after NOx adsorption and nitrites hydrogenation, and the whole process is conducted under ambient conditions without additional heating operation.

Since the NOx transformation into nitrite is easily achieved through adsorption in alkaline solution, the key point of research in this approach concentrates on precisely regulating the product selectivity of nitrite hydrogenation and designing efficient nitrite hydrogenation catalyst under versatile conditions. As shown in reactions (2)-(4), we initially investigated the hydrogenation mechanism to inhibit the side reaction pathway, which provided clues for the catalyst design. Some previous studies have reported that noble metal catalysts could hydrogenate nitrate or nitrite into ammonia or N2 [21-23], as noble metal catalysts such as palladium (Pd) could provide active hydrogen (H) species through facile hydrogen dissociation [24], Nevertheless, to design a desired catalyst and selectively reduce nitrite into ammonia still remain a grand challenge. Enlightened by synergy cooperation between single atom sites and nanoparticle species [25-27], we combined theoretical and experimental studies to design a Pd single atom/nanoparticle co-existence catalyst with CTF as the support [28–31] for its rich porous structure and excessive N structure to anchor metal species. The desired catalytic synergy between Pd<sup>2+</sup> and Pd<sup>0</sup> in this catalyst improved the nitrite conversion to 100% and the ammonia selectivity to ~100% without other detected byproducts. C<sub>3</sub>N<sub>4</sub> [32] and SiO<sub>2</sub> [33] which possess porous structures and different functional groups, were chosen as supports for control experiments to estimate the influence of Pd distribution and coordination on the catalytic activity and selectivity.

#### 2. Experimental

#### 2.1. Preparation of catalysts

The preparation of CTF employed an ionothermal synthesis method described in previous reports [34-36]. First, 2, 6-dicyanopyridine and zinc chloride (ZnCl2) were ground in a glovebox according to a weight ratio of 3 g/15.9 g, and then the mixture was sealed in a quartz tube with a spacious antrum under vacuum conditions. The sealed mixture was then calcined in a muffle furnace at 400 °C for 20 h and 600 °C for 20 h with a ramping rate of 2 °C/min, since 600 °C was conducive to improving the surface area of CTF. Afterward, the generated black solid was washed 5 times by hot water to remove the residual ZnCl<sub>2</sub>, followed by intense stirring in hydrochloric acid solution (2 M) and filtration. Finally, the obtained sample was washed by deionized water/tetrahydrofuran (THF) several times and dried in a vacuum oven overnight at 100 °C. In addition to CTF, C<sub>3</sub>N<sub>4</sub> and SiO<sub>2</sub> were chosen as references to elucidate the palladium-support interaction on metal dispersion and activity. The C<sub>3</sub>N<sub>4</sub> support was prepared based on a previously reported procedure [37], which was synthesized by a functional NaHCO3 template-mediated synthesis strategy. The SiO2 support was purchased from Beijing Mreda Technology INC and used directly without other treatment.

Herein, the Pd species were introduced to supports through impregnation method and  $Pd^{2+/0}/CTF$  was exemplified to explain the procedure. First, 500 mg CTF and 82.5 mg of Pd(TFA) $_2$  were added into 20 mL deionized water and stirred for 12 h at RT under  $N_2$  protection. Then, the suspension was filtered and washed by deionized water several times. The solid product was finally dried in a vacuum oven and pretreated with  $H_2$  at 350  $^{\circ}\text{C}$  for 15 min prior to the reaction.

#### 2.2. Characterization

X-ray diffraction (XRD) was recorded on an Empyrean-100 X-ray diffractometer with a Cu K $\alpha$  radiation source ( $\lambda=1.541$  Å) at 40 mA and 40 kV in the range of  $10^\circ-90^\circ$ .  $N_2$  isotherms were obtained at 77 K on a Quantachrome autosorb iQ2 gas adsorption analyzer. Prior to the test, all samples were degassed at 250 °C for 8 h. The Pd loading was determined by inductively coupled plasma atomic emission spectrometry (ICP-OES, Varian Vista Axial Instrument), while the N and C contents were examined through an organic element analyzer (Elementar vario EL cube, Germany). Transmission electron microscopy (TEM,

TECNAI G2 F20 200 keV, USA) was used to investigate the morphology and noble metal dispersion. Atomic resolution high-angle annular dark-field scanning transmission electron microscopy (HAADF-STEM) images were obtained on an FEI Titan STEM/TEM microscope equipped with a probe corrector. Before imaging, the powder was dissolved in anhydrous ethanol and lightly dusted onto 230 mesh Cu grids coated with ultrathin carbon membrane.

 $H_2$ -TPR and CO pulse were conducted on a Micromeritics AutoChem II 2920 with TCD as the detector. Prior to the  $H_2$ -TPR measurement, 0.1 g sample was pretreated with Ar at 200 °C for 60 min, and then the temperature was elevated from 50 °C to 550 °C under 5%  $H_2$ /Ar at a rate of 10 °C • min $^{-1}$ .  $Pd^{2+}/Pd^{0}$  ratios can be calculated by the  $Pd^{2+}$  loading through  $Pd^{2+}$  reduction peak integral with assistance of quantification function from facility and the total Pd loading from ICP test. Before the CO pulse test, 0.1 g sample was pretreated with 5%  $H_2$ /Ar at 300 °C for 3 min, and the CO pulse was conducted at 30 °C. X-ray photoelectron spectroscopy (XPS) was performed on a Thermo escalab 250Xi by using an Al Ka radiation source operating at 1486.6 eV. The binding energy and the Auger kinetic energy scales were referenced to the C 1 s signal at 284.6 eV from adventitious carbon. TGA was conducted on a NETZSCH thermogravimetric analyzer (STA 449 F5) equipped with a Mettler-Toledo balance, and the detailed inlet composition was shown in the results

Diffuse reflectance infrared Fourier transform spectroscopy (DRIFTS) were conducted on a Bruker VERTEX 70 V equipped with an MCT detector and a high-temperature reaction chamber (Spectra-Tech collector) with ZnSe windows. The chamber was connected to a gas-distributing system. To eliminate the interference from water, the samples were initially pretreated with Ar in an infrared drying oven for 0.5 h to remove adsorbed water before each experiment. The DRIFTS spectra were collected in the range of 650–4000 cm $^{-1}$  with a resolution of 4 cm $^{-1}$ . Prior to each test, the powder sample was pretreated with Ar at 200  $^{\circ}$ C for 0.5 h, and its absorbance spectra were collected at RT as the background. Before the hydrogenation reaction, NaNO2 was impregnated on CTF-Pd according to a weight ratio of 6.89:80.

#### 2.3. Activity test

The NOx conversion into ammonia involves three steps, as shown in Scheme 1b: (a): NOx adsorption. This work utilized a NaOH solution (pH=13~14) to adsorb and convert NO/NO<sub>2</sub> into nitrite under RT and atmospheric pressure. The NO/NO<sub>2</sub> ratio in the inlets was 1:1, and the flow rate was 20 mL/min. The adsorption process used 20 mL of NaOH solution as an adsorbent, and this process was maintained for 90 min to quantify the nitrate and nitrite concentrations by ion chromatography (IC) with conductivity detection (Thermo Fisher Scientific ICS-6000 system; ASRS Recycle mode; Ionpac AS11-HC column; 20 mM KOH as the eluent; 1 mL/min eluent flow rate). b): Direct nitrite hydrogenation into ammonia. Quantified the ammonia concentrations by ion chromatography (IC) with conductivity detection, (Thermo Fisher Scientific ICS-6000 system; CSRS Recycle mode; Ionpac CS12A column; 20 mM methanesulfonic acid as the eluent; 0.6 mL/min eluent flow rate) and an external standard (NH<sub>4</sub>Cl as the external standard). Two milliliters of deionized water, 1 mmol of sodium nitrite (NaNO2) and 80 mg of catalyst were added to a branched 15 mL glass tube. H2 was supplied by a gasbag connected to the branch, and the whole suspension system was blended for 24 h under ambient conditions. The products were quantified by IC and external standard methods. In the cyclic activity test, the catalyst was filtered and washed with deionized water, and the dried catalyst was reused again without any pretreatment. (c): Ammonia desorption. To estimate ammonia release from the reaction system as a model test, the product solution was heated to 50 °C, and the temperature was maintained for 3 h. The residual ammonia concentration was quantified by IC.

#### 2.4. Density functional theory (DFT) calculations

The geometry optimizations and frequency calculations were carried out using the B3LYP functional [38-40]. The van der Waals correction of Grimme's D3 scheme with Becke-Johnson damping (DFT-D3 (BJ)) was incorporated to describe the noncovalent interactions between the adsorbent and the adsorbate [41,42]. The 6-31 G (d,p) basis set was used for the nonmetal atoms (C, H, O and N), and the SDD effective core potential was used for the Pd atoms. For each geometric stationary point, the single-point energy calculations were performed using an extended 6-31 + +G(d,p) basis set for the nonmetal atoms the SMD solvation model to determine the effect of the solvent (water) [43]·H<sub>3</sub>O<sup>+</sup> was used as the proton donor in the calculations. The binding free energy ( $G_b$ ) was calculated as follows:  $G_b = G_{Pd-NO2} - G_{Pd} - G_{NO2}$ , where G<sub>Pd-NO2</sub> is the free energy of the complex consisting of the Pd catalyst model and nitrite, and  $G_{\text{Pd}}$  and  $G_{\text{NO2}}$  are the free energies of the Pd catalyst model and nitrite respectively. All the calculations were performed with the Gaussian 16 software package [44].

#### 3. Results and discussion

#### 3.1. DFT calculation of nitrite hydrogenation over Pd catalyst

Since  $N_2$  is found to be the dominating nitrate/nitrite hydrogenation product previously, the simulation of nitrite hydrogenation is initially conducted to guide the catalyst design and preparation to improve the ammonia selectivity specifically. According to theoretical predictions of binding free energies  $(G_b)$ , nitrite ions  $(NO_2^1)$  adsorbs on single  $Pd^{2+}$  atoms (-1.13 eV) more easily than on  $Pd_{13}$  (-0.80 eV) and single  $Pd^0$  atoms (-0.42 eV) (see Fig. 1b), illustrating the preferential capture sites of nitrite on the  $Pd^{2+}$  species during hydrogenation. To verify the results through B3LYP functional, TPSS and PBE0 functionals have been employed to optimize the geometry of  $Pd_{13}$  cluster. The interactions between small molecules  $(H_2$  and nitrite) and two Pd-based adsorbents  $(Pd_{13}$  cluster and  $Pd^{2+}$  atom) were investigated subsequently, using TPSS and PBE0.

The calculated  $G_b$  also indicates nitrite adsorbs on single  $Pd^{2+}$  atoms more easily than on Pd<sub>13</sub>, as shown in Table S1. Because B3LYP is suitable to calculate the hydrogenation processes of  $NO_2^-$ @Pd $^{2+}$  model, only B3LYP is used in the subsequent calculations. Similar to the H2 dissociation on the Pd(111) surface, the H-H bond of H2 can be broken easily without an energy barrier when H<sub>2</sub> is located on the Pd<sub>13</sub> cluster. Therefore, hydrogen dissociation is likely dominant on the Pd nanoparticles in the presence of H<sub>2</sub>. The migration of highly active H atoms from Pd<sub>13</sub> cluster to the substrate material could help trigger the hydrogenation reaction of \*NO<sub>2</sub> on the Pd<sup>2+</sup> sites. As shown in Fig. 1c, the hydrogenation process starts from the conversion of \*NO2 to \*NO, in which the N-O bond is broken by one H atom and proton, yielding H<sub>2</sub>O, and this reaction is an exothermic process (-0.55 eV). Since the isolated Pd<sup>2+</sup> single-atom sites provides only one reactive site, the dissociation of N-O to \*N and \*O can be avoided, which may occur with the aid of adjacent active sites on the Pd surface. Consequently, the dissociation pathway is not included in the theoretical investigations. The most likely hydrogenation product of \*NO in ammonia synthesis is \*HNO. The freeenergy changes revealed that this process is slightly endothermic (0.30 eV). Furthermore, the next hydrogenation of \*HNO can be achieved through H attachment to the O atom, and the  $\Delta G$  of this process (\*HNO → \*HNOH) is only 0.23 eV. The remaining hydrogenation reactions in ammonia formation, including the formation of two intermediate species (\*H2NOH and \*NH2), are exothermic processes. In N2 synthesis, \*NO hydrogenation to \*NOH and the following conversion to \*N are both endothermic processes (1.24 and 1.47 eV). In addition, the conversion of \*N2O to \*N2OH presents the highest energy increase of 1.32 eV. The DFT calculations reveal that N2 formation is much more difficult than ammonia formation on the Pd<sup>2+</sup> sites, therefore, the designed catalyst possessing Pd<sup>2+</sup> single atoms and Pd nanoparticles is

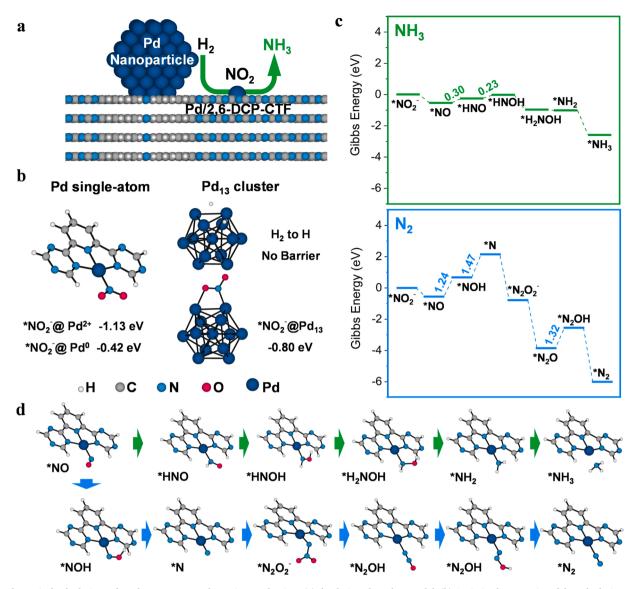


Fig. 1. Theoretical calculations of catalyst structure and reaction mechanism. (a) The designed catalyst model. (b) Optimized geometries of the calculation models of the  $Pd^{2+}$  single-atom catalyst ((2,6-di(1,3,5-triazin-2-yl)pyridine) palladium(2 +/0)) and the Pd nanocatalyst ( $Pd_{13}$  cluster). The values shown are the binding free energies between nitrite and the  $Pd^{2+}/Pd^0$  single-atom model, and between nitrite and the  $Pd_{13}$  cluster. (c) Free energy diagram of the minimum energy pathway for ammonia and  $Pd^{2+}/Pd^0$  single-atom model, and between the differences in the reaction free-energies in each pathway. Other possible reaction pathways for the final products of ammonia and  $Pd^2$  are shown in  $Pd^2$  shown in  $Pd^2$ 

likely to increase the ammonia selectivity. Moreover, the minor endothermic processes in the ammonia pathway imply that selective hydrogenation can occur under ambient conditions.

## 3.2. Characterization of Pd distribution and hydrogenation performance over Pd based catalysts

According to the above mechanism, the designed  $Pd^{2+/0}/CTF$  was synthesized, and  $Pd^{2+/0}/C_3N_4$  [32] and  $Pd^{2+/0}/SiO_2$  [33] were chosen as reference to estimate their nitrite conversion and ammonia selectivity. Table 1 displays the compositions and SSA results of Pd-based catalysts. CTF presented the highest SSA of 1349.968  $m^2/g$ , and the Pd loading decreased the SSA of all catalysts compared with the corresponding supports. In addition, the ICP results showed that the Pd contents were 4.9 wt%  $(Pd^{2+/0}/CTF)$ , 4.6 wt%  $(Pd^{2+/0}/SiO_2)$  and 4.3 wt%  $(Pd^{2+/0}/C_3N_4)$ . In addition, the available N and C contents are also summarized in Table 1 to analyze Pd surface enrichment later.

The  $N_2$  adsorption-desorption isotherms in Fig. 2a and pore size distribution shown in Fig. 2b suggested the rich microporous structure

**Table 1**The specific surface area (SSA) and compositions of all samples.

Sample	SSA (m <sup>2</sup> /g)	Pd/N/C contents (wt %)	Sample	SSA (m <sup>2</sup> /g)	Pd/N/C contents (wt %)
CTF	1349.9	0/7.09/46.37	Pd/CTF	1113.3	4.9/7.58/ 43.14
$SiO_2$	177.6	/	Pd/SiO <sub>2</sub>	161.0	4.6/0/0
$C_3N_4$	52.6	0/59.70/ 33.96	Pd/ C <sub>3</sub> N <sub>4</sub>	29.1	4.3/56.79/ 32.3

of CTF support, while  $SiO_2$  and  $C_3N_4$  exhibited meso-(macro)-porous structures, as shown in Fig. 2b. Moreover, the Pd loading decreased the amount of  $N_2$  adsorption amount compared with corresponding pristine supports, but the pore distribution was not affected, implying that the Pd particles blocked partial pore structure. The XRD profiles in Fig. 2c are used to identify the material phases. The synthesized  $C_3N_4$  exhibited typical peaks at  $28^\circ$ ,  $47^\circ$  and  $57^\circ$  [37], and the peaks at  $41^\circ$  and  $83^\circ$  in

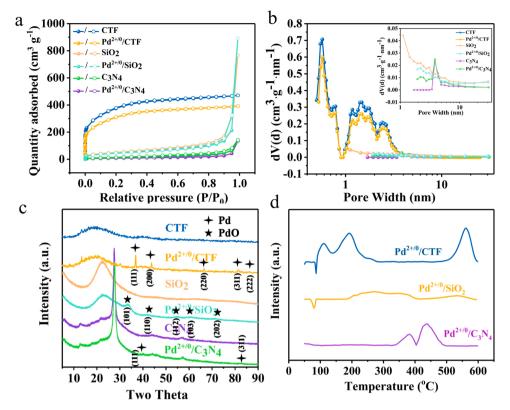


Fig. 2. (a)  $N_2$  adsorption-desorption isotherms of CTF,  $Pd^{2+/0}/CTF$ ,  $SiO_2$ ,  $Pd^{2+/0}/SiO_2$ ,  $C_3N_4$  and  $Pd^{2+/0}/C_3N_4$ . (b) Pore distribution of CTF,  $Pd^{2+/0}/CTF$ ,  $SiO_2$ ,  $Pd^{2+/0}/SiO_2$ ,  $C_3N_4$  and  $Pd^{2+/0}/C_3N_4$ . (c) XRD profiles of CTF,  $Pd^{2+/0}/CTF$ ,  $SiO_2$ ,  $Pd^{2+/0}/SiO_2$ , P

the XRD pattern of  $Pd^{2+/0}/C_3N_4$  were ascribed to the Pd diffraction peaks. The commercial  $SiO_2$  support presented typical broad peaks at  $23.8^{\circ}$  and  $45^{\circ}$ , and PdO diffraction peaks at approximately  $34^{\circ}$ ,

 $42^\circ, 55^\circ, 61^\circ$  and  $71^\circ$  were recorded. The Pd diffraction peaks of the Pd^2+/0/CTF sample at approximately  $41^\circ, 47^\circ, 69^\circ, 83^\circ$  and  $86^\circ$  were also recorded. The various Pd species indicated from the XRD diffraction peaks suggested the support greatly affected the Pd distribution and locations.

Since the crystallinity of the synthesized CTF support was inferior, more methods were used to identify its framework structure. The XPS spectra in Fig. S2 presented three N 1 s XPS peaks corresponding to pyridinic N (398.3 eV), pyrrolic N (401 eV) and graphitic N (403.9 eV). The C 1 s XPS spectra in Fig. S3 showed three peaks at 284.5 eV, 286.5 eV and 288.4 eV, assigned to C-C, C-N and graphitized carbon, respectively [45]. These structures confirmed the formation of the triazine ring structure, and high-temperature calcination indeed caused the generation of a graphite phase, leading to partial skeleton collapse. The IR spectra in Fig. S4 presented the disappearance of the peaks corresponding to the monomers at approximately 3075 cm<sup>-1</sup> (C-H stretching vibration) and 2245 cm<sup>-1</sup> (ascribed to the -CN stretching vibration in the conjugated nitrile), illustrating the consumption of 2, 6-dicyanopyridine. In the spectra of the synthesized products, the appearance of peaks at 1180 cm<sup>-1</sup> and 1560 cm<sup>-1</sup> confirmed the formation of triazine ring structure, and Pd loading did not induce any new peaks, which only weakened the peak intensities at 1180 cm<sup>-1</sup> and 1560 cm<sup>-1</sup> [46].

Figs. 3a-3f showed the Pd distribution through TEM and HAADF-STEM images.  $Pd^{2+/0}/CTF$  and  $Pd^{2+/0}/SiO_2$  presented uniform particle sizes below 5 nm (statistical results were shown in the inset), while  $Pd^{2+/0}/C_3N_4$  possessed larger Pd nanoparticles between 2 and 25 nm. Massive light spots were detected in the HAADF-STEM images of  $Pd^{2+/0}/CTF$  and  $Pd^{2+/0}/C_3N_4$ , ascribed to atomically dispersed Pd species, but not in the images of the  $Pd^{2+/0}/SiO_2$ . The Pd dispersion estimated from

the CO pulse was 32.4%, 36.7% and 44.3% for  $Pd^{2+/0}/CTF$ ,  $Pd^{2+/0}/SiO_2$  and  $Pd^{2+/0}/C_3N_4$ , respectively. Although it seemed controversial for the Pd dispersion from the CO pulse result and TEM image for  $Pd^{2+/0}/C_3N_4$ , it was confirmed that electron irradiation easily induced the  $C_3N_4$  support to melt and generated larger Pd slices, as shown in the TEM image. The weak Pd diffraction peaks in Fig. 2c also suggested that the Pd nanoparticle sizes were comparable to those of the other two samples. Therefore, the Pd distribution throughout  $Pd^{2+/0}/C_3N_4$  was the highest, as the CO pulse result showed.

The  $H_2$ -TPR plots of the  $Pd^{2+/0}/CTF$  sample shown in Fig. 2d presented three  $Pd^{2+}$  reduction peaks at approximately 120 °C, 200 °C and 550 °C. Nevertheless, the  $Pd^{2+}$  reduction temperature over  $Pd^{2+/0}/C_3N_4$  and  $Pd^{2+/0}/SiO_2$  shifted to higher temperatures, especially for the  $Pd^{2+/0}/C_3N_4$  sample, illustrating their inferior reducibility and the much stronger interaction between the  $Pd^{2+}$  and the supports. Likewise, the XPS spectra in Fig. S5-S7 revealed the coexistence of  $Pd^{2+}$  and  $Pd^{0}$  over the catalyst surface. The signals at binding energies of 337.9 eV and 343.2 eV were assigned to  $Pd^{2+}$  3d<sub>5/2</sub> and 3d<sub>3/2</sub>, and those at 335.7 eV and 340.9 eV were ascribed to  $Pd^{0}$  3d<sub>5/2</sub> and 3d<sub>3/2</sub> [52,53]. Peak fitting and area integration were performed, and the  $Pd^{2+}/Pd^{0}$  ratios from  $Pd^{2+}/Pd^{0}$  ratios are showed in Fig. 3i. The  $Pd^{2+/0}/CTF$  exhibited the highest  $Pd^{2+}/Pd^{0}$  ratio, while  $Pd^{2+/0}/C_3N_4$  exhibited the lowest ratio. To date, the impact of the support structure on the Pd distribution and valence states has been well analyzed.

Pd K-edge XANES were conducted to confirm the locations of Pd species and their charge. The experimental evidences are shown in Fig. 4 and Table S2. The white line intensity of Pd over  $Pd^{2+/0}/CTF$  in Pd K-edge XANES profiles is between Pd foil and PdO (Fig. 4a), and the adsorption edge in the inset also locates between Pd foil and PdO, demonstrating the Pd charge over  $Pd^{2+/0}/CTF$  is between  $0\sim2$  (but close to  $Pd^{2+}$ ). The FT k3-weighted EXAFS spectra in R space of  $Pd^{2+/0}/CTF$  exhibit two obvious peaks (Fig. 4b). The first one at 1.94 Å represents the Pd-N coordination with coordination number of 3, proving the

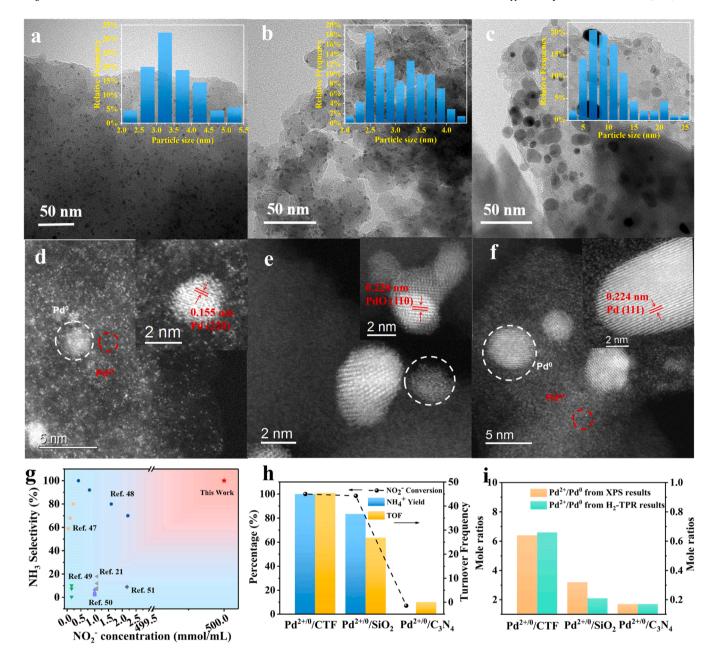


Fig. 3. Catalysts structure characterization and catalytic performance. TEM images of (a)  $Pd^{2+/0}/CTF$ . (b)  $Pd^{2+/0}/SiO_2$  and (c)  $Pd^{2+/0}/C_3N_4$  and atomic-resolution HAADF-STEM images of (d)  $Pd^{2+/0}/CTF$ . (e)  $Pd^{2+/0}/SiO_2$  and (f)  $Pd^{2+/0}/C_3N_4$ . The scale bar in the TEM images represents 50 nm. (g) Ammonia selectivity as a function of nitrite concentration during hydrogenation. The data from the same reference were labeled by symbols of the same color [21, 47–51]. (h) The ammonia yield, nitrite conversion and the related TOF over three catalysts (TOF calculation is based on Pd loading from ICP and Pd dispersion from TEM results); (i)  $Pd^{2+}/Pd^0$  ratios calculated from the XPS and  $Pd^2$ -TPR results.

existence of atomically dispersed  $Pd^{2+}$  sites. The other one at 2.92 Å is assigned to the Pd-Pd coordination with coordination number of 4, illustrating the formation of Pd particles on catalyst. And the triple-coordination between Pd and N benefited its catalytic reactivity during thermo-catalysis process.

In addition, the ammonia yield and TOF comparison under ambient conditions are shown in Fig. 3 h, and the concentrations of nitrite and ammonia in solution were quantified by ion chromatography (IC).  $Pd^{2+/0}$ /CTF catalyzed 100% of the nitrite into ammonia according to the detected N-containing products, but  $Pd^{2+/0}/SiO_2$  and  $Pd^{2+/0}/C_3N_4$  presented much lower ammonia yields of 83.4% and 0.2%, respectively. Fig. 3g shows a comparison between the activities of catalysts in this work and those reports in previous literatures. The comparison revealed that the ammonia yield over the designed  $Pd^{2+/0}/CTF$  sample was

superior considering to the reactant concentration. Table S3 also listed the nitrite conversion as a function of pH value in solution, and  $Pd^{2+/0}/CTF$  exhibited desired hydrogenation performance all the time. Consequently, the nitrite concentration was hundred times higher than previous literatures and the pH environment herein was versatile, directly affecting the energy utilization efficiency and operation costs during its scalability. Besides, even though the reaction conditions were completely different, the ammonia generation efficiency over  $Pd^{2+/0}/CTF$  was still higher than recent ammonia generation report using photoelectrochemical NOx conversion over TiOx/CdS/CZTS catalyst under mild conditions [54].

To determine the reaction products other than ammonia that formed during the hydrogenation process over Pd<sup>2+/0</sup>/CTF, the effluent components of the reaction system were monitored by online mass

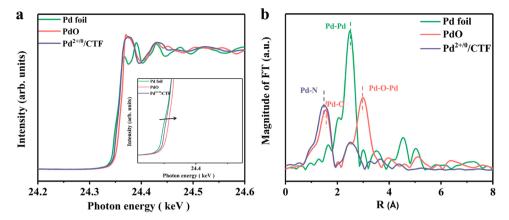


Fig. 4. (a) Pd K-edge XANES spectra for  $Pd^{2+/0}/CTF$ . Pd foil and PdO were used as the references. (b) Pd K-edge EXAFS in R space for  $Pd^{2+/0}/CTF$ . Pd foil and PdO were used as the references.

spectrometry (MS). Fig. S8 lists the  $\rm H_2$ , NH $_3$  and N $_2$  concentrations as a function of reaction time, and the system was purged with H $_2$  as the reactant. The dramatic initial fluctuation of H $_2$  and N $_2$  was induced by the valve switch. The results demonstrated that only the ammonia concentration rose until it stabilized with time on stream, illustrating the generation of ammonia and ammonia release during this process, while the N $_2$  concentration remained constant throughout the reaction. In addition, the scanning mode of the mass number showed signals of 2 (H $_2$  reactant), 4 (He carrier gas), 15(NH), 17 (NH $_3$ ), and 18 (H $_2$ O as solvent), but peaks corresponding to N $_2$  (28), NO (30), N $_2$ O (44) and NO $_2$  (46) were not detected (Fig. S9 and 10). Besides, the isotope experiments with  $^{15}$ NO $_2$  as reactants for hydrogenation was also performed over Pd $^{2+/0}$ /CTF, and the NMR spectra (Fig. S11) proved the N atoms all originated from  $^{15}$ NO $_2$  but not N from CTF framework.

As proposed in Fig. 1c, the Pd<sup>0</sup> and Pd<sup>2+</sup> species were the major active sites for H<sub>2</sub> dissociation and nitrite hydrogenation, and the rate determining step was NO\* generation from nitrite dissociation during the ammonia synthesis. Since Pd<sup>2+/0</sup>/CTF presented the highest activity and the optimal Pd<sup>2+</sup>/Pd<sup>0</sup> distribution among the three Pd-based samples, the effect of Pd<sup>2+</sup>/Pd<sup>0</sup> ratios on ammonia selectivity over the Pd<sup>2+</sup>/ /CTF sample was estimated. The contrast experiments were performed on oxidized/reduced Pd<sup>2+/0</sup>/CTF to exaggerate the Pd<sup>2+</sup>/Pd<sup>0</sup> ratio through  $O_2$  (H2) treatment at 300  $^{\circ}\text{C}$  (350  $^{\circ}\text{C})$  for 40 min (6 h) prior to nitrite hydrogenation on the conditions of intact CTF structure (oxidized: Pd<sup>2+</sup>/CTF, reduced: Pd<sup>0</sup>/CTF). Compared with that of the pristine Pd<sup>2+/0</sup>/CTF sample, the Pd<sup>2+</sup> reduction peaks in the H<sub>2</sub>-TPR plot disappeared below 400 °C, as shown in Fig. S12, proving the partial reduction of Pd<sup>2+</sup> to Pd<sup>0</sup> over Pd<sup>0</sup>/CTF, while the Pd<sup>2+</sup> reduction peaks became larger in the plot of Pd<sup>2+</sup>/CTF. Similarly, the XPS results shown in Fig. S13-S14 also proved the increase of Pd2+ ratio on Pd2+/CTF and the decrease of Pd<sup>2+</sup> ratio on Pd<sup>0</sup>/CTF (see Table S4). Consequently, as shown in Fig. S15, nitrite hydrogenation tests exhibited 84% nitrite conversion and 54% ammonia selectivity over Pd<sup>0</sup>/CTF and 79% nitrite conversion and 11% ammonia selectivity over Pd<sup>2+</sup>/CTF. For the Pd<sup>0</sup>/ CTF sample, the decline in Pd<sup>2+</sup> boosted the N<sub>2</sub> generation on Pd<sup>0</sup> sites in the presence of excess dissociated H atoms, while the shortage of Pd<sup>0</sup> over Pd<sup>2+</sup>/CTF greatly inhibited H atom production and induced a clear decrease in the ammonia yield over the Pd<sup>2+</sup> sites, which proved that the Pd<sup>0</sup> species preferentially generated N<sub>2</sub> and the Pd<sup>2+</sup>/Pd<sup>0</sup> ratio dominated the product dispersion. Similarly, the MS signal obtained in the mass scanning mode during this process provided evidence of N2 generation, as shown in Fig. S16-S17. Since the CTF structure collapses quickly above 350 °C, as shown in Fig. S18-S19, complete reduction of  $Pd^{2+/0}/CTF$  was not performed above 350 °C.

The DRIFTs of nitrite hydrogenation in the presence of 6% water over  $Pd^{2+/0}/CTF$  were also showed in Figs. 5a-5c to demonstrate the influence of  $Pd^{2+}/Pd^0$  ratio on the detected reaction intermediates.

During the nitrite hydrogenation process, a peak appeared at approximately  $1032~\rm cm^{-1}$ ; which represented the nitrites on the  $Pd^{2+/0}/CTF$  samples, and its decrease with the introduction of  $H_2$  into the system illustrated its gradual consumption. The appearance of peaks at approximately  $1023~\rm cm^{-1}$  and  $1054~\rm cm^{-1}$  was ascribed to -NO\* species and -NH $_3$  species [55,56], and the appearance of -NH $_3$  species always occurred after the -NO\* species formed over three  $Pd^{2+/0}/CTF$  samples, which was consistent with the ammonia generation rationale shown in Fig. 1c. New peaks appeared at 2830 and 2941 cm $^{-1}$  and were assigned to the N-H

stretching mode of the generated ammonia ions [57]. In addition, only Pd<sup>2+/0</sup>/CTF presented stronger NH<sub>3</sub> peaks at 1054 cm<sup>-1</sup> than the Pd<sup>2+</sup>/CTF (Pd<sup>0</sup>/CTF) samples, since Pd<sup>2+/0</sup>/CTF showed an ammonia yield that was superior to the yields of the others. Thus far, due to the contrast between Pd<sup>2+</sup>/Pd<sup>0</sup> ratios and ammonia yield in Figs. 3i and 3 h over three samples, it was concluded that the ammonia yield was not only determined by optimal coordination but also the desired Pd<sup>2+</sup>/Pd<sup>0</sup> ratios during nitrite hydrogenation. Furthermore, the Pd/C ratio or Pd/N ratio identified by XPS and ICP, as shown in Table S5 indicated that Pd was enriched on the catalyst surface, since XPS mainly characterized elements on the sample surface. The surface enrichment of Pd species benefited the mass transfer of reactants during the heterogeneous reaction system, which could expel the impact of pore structure on the activity results among various catalysts. Generally speaking, the efficient cooperation between Pd2+ and Pd0 during hydrogenation greatly relied on their location and reducibility on the supports. The structural investigations of CTF, SiO2 and C3N4 revealed that the Pd<sup>2+/0</sup>/CTF possessed triazine groups and anchored Pd<sup>2+</sup> and Pd<sup>0</sup> species around N atoms, exhibiting the highest reducibility. The layered structure of C<sub>3</sub>N<sub>4</sub> sealed the Pd<sup>2+</sup> and Pd<sup>0</sup> species tightly and presented inferior activity, and SiO2 contained only Pd nanoparticles. The shortage of atomically dispersed Pd species led to moderate hydrogenation reactivity under ambient conditions.

### 3.3. The stability test of $Pd^{2+/0}/CTF$ and the bench test from NOx into ammonia

Fig. 6 presents the catalytic stability of  $Pd^{2+/0}/CTF$  through cyclic activity test. Throughout the 8 cycle evaluations, the ammonia selectivity was maintained at  $\sim 100\%$ , while the nitrite conversion maintained around 90% after 5 cycle's reaction. Fig. 6c presented.

the XRD profiles of the used  $Pd^{2+/0}/CTF$  sample. Typical Pd (111) and (200) peaks were detected for all samples, and their peak intensities did not increase clearly. In Fig. 6d, the TEM images of fresh and used  $Pd^{2+/0}/CTF$  samples showed an increased Pd particle size, which was partially responsible for the activity decrease in Fig. 6a. In addition, the ICP test of Pd revealed 5.0 wt% content on used  $Pd^{2+/0}/CTF$  samples,

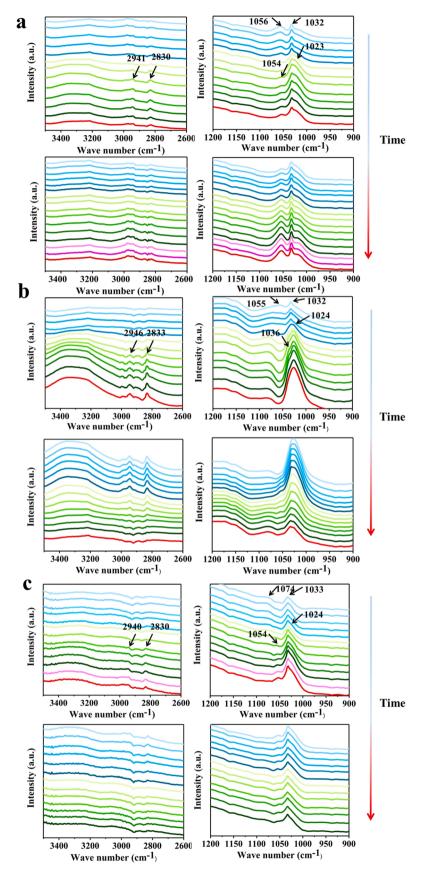


Fig. 5. DRIFTS spectra of nitrite hydrogenation over (a)  $Pd^{2+/0}/CTF$ , (b)  $Pd^{2+}/CTF$  and (c)  $Pd^{0}/CTF$  under ambient conditions.

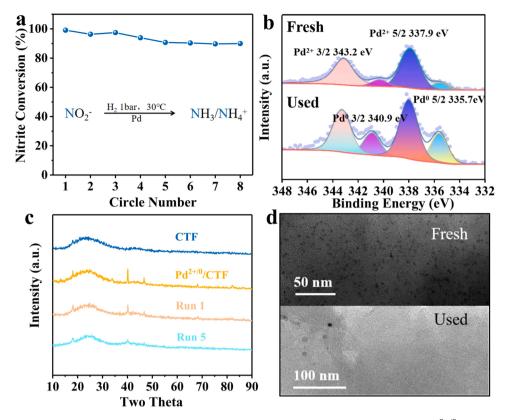


Fig. 6. The catalytic stability evaluation and corresponding bulk characterization of spent catalyst. (a) Cycle stability over  $Pd^{2+/0}/CTF$ ; (b) the XPS spectra of Pd 3d over fresh and used  $Pd^{2+/0}/CTF$ ; (c) XRD profiles of CTF,  $Pd^{2+/0}/CTF$  and used  $Pd^{2+/0}/CTF$  samples; (d) TEM images of fresh and used  $Pd^{2+/0}/CTF$  after the hydrogenation reaction.

illustrating no Pd leaching during reaction process. As the XPS spectra of the fresh and used  $Pd^{2+/0}/CTF$  in Fig. 6b, the used  $Pd^{2+/0}/CTF$  after 8 cycles also revealed Pd<sup>0</sup> and Pd<sup>2+</sup> signals, but the Pd<sup>2+</sup>/Pd<sup>0</sup> ratio decreased from 6.4 to 2.3, demonstrating the gradual reduction of Pd<sup>2+</sup> on the sample surface during the hydrogenation reaction, which led to Pd aggregation and was also responsible for the decreased activity shown in Fig. 6a. Finally, a model test was conducted to estimate the overall NOx conversion efficiency including single-pass NOx saturated adsorption in NaOH solution and subsequent Pd<sup>2+/0</sup>/CTF hydrogenation in 24 h. The results presented in Fig. S18 show that 70% NOx could be converted into nitrite under a gas flow rate of 20 mL/min, and the subsequent hydrogenation using Pd<sup>2+/0</sup>/CTF as a catalyst under ambient conditions could achieve 100% conversion of nitrite into ammonia. This model test clearly presented satisfactory ammonia synthesis efficiency, and the emitted NOx issue could be solved by continuous cycle adsorption.

#### 4. Conclusion

In this work, we pioneer a new approach for NOx recycling through the hydrogenation of nitrite into ammonia, and the designed and screened out Pd<sup>2+/0</sup>/CTF catalyst exhibits a state-of-the-art ammonia yield. The DFT results initially pointed out the NO\* was a key intermediate and its hydrogenation into \*HNO or \*NOH would lead to generation of ammonia or N<sub>2</sub> in products, respectively. Meanwhile, the Pd<sup>2+</sup> and Pd<sup>0</sup> species were necessary for nitrite hydrogenation and H<sub>2</sub> dissociation. The subsequent catalysts preparation successfully loaded Pd<sup>2+</sup> and Pd<sup>0</sup> species through fabricating single atom Pd sites and Pd nanoparticles simultaneously on CTF support, and SiO<sub>2</sub> and C<sub>3</sub>N<sub>4</sub> were also utilized to examine the influence of Pd-supports interaction on hydrogenation performance. The bulk characterization demonstrated Pd/CTF possessed the highest Pd<sup>2+</sup>/Pd<sup>0</sup> ratios (6.4:1), and exhibited 100%

nitrite conversion with 100% ammonia selectivity under ambient condition. Through the comparison of Pd distribution and electronic properties among various catalysts, the easily reduced Pd<sup>2+</sup> species on CTF support and the optimal Pd<sup>2+</sup>/Pd<sup>0</sup> ratios enhanced the nitrite hydrogenation efficiency. The variation of  $Pd^{2+}/Pd^{0}$  ratios on  $Pd^{2+}/CTF$  (1:0) and Pd<sup>0</sup>/CTF (0.57:1) decreased ammonia yield and illustrated excessive Pd<sup>0</sup> species benefited N<sub>2</sub> generation during nitrite hydrogenation. The DRIFTs of nitrite hydrogenation proved the generation of NO\* and only Pd $^{2+/0}$ /CTF revealed stronger NH $_3$  peaks at 1054 cm $^{-1}$  than the Pd<sup>2+</sup>/CTF (Pd<sup>0</sup>/CTF) for its superior performance on ammonia yield. The final model test revealed 70% NOx could be adsorbed by NaOH solution from single pass, and the Pd<sup>2+/0</sup>/CTF catalyst achieved 100% nitrite conversion into ammonia without byproducts. The subsequent ammonia desorption could be completely achieved at 50 °C under heating condition and the NaOH solution is recycled as absorbent without pollutant emission. Moreover, the Pd<sup>2+/0</sup>/CTF catalyst still retained high catalytic activity when recycled 8 times. It presents satisfactory catalytic stability and gives a desired ammonia synthesis route from nitrite hydrogenation.

#### CRediT authorship contribution statement

W.D. conceived the concept and designed the research. J.Y. prepared the catalysts and carried out characterization measurements and activity tests. T.Y. carried out sample characterization, analyzed the results and wrote the first draft. L.S. conducted DFT calculations and wrote the corresponding section of the manuscript. X.F., S.Z., L.Z., G.R., R.T., D.Z. and Z.L. all discussed the results and help edit the manuscript.

#### **Declaration of Competing Interest**

The authors declare that they have no known competing financial

interests or personal relationships that could have appeared to influence the work reported in this paper.

#### Data availability

Data will be made available on request.

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#### Appendix A. Supporting information

Supplementary data associated with this article can be found in the online version at doi:10.1016/j.apcatb.2023.122548.

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